

Detailed study of superconductivity in nanostructured nanocrystalline boron doped diamond thin films

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In this paper, we report on the transport properties of nanostructured boron doped diamond thin films. The nanostructures made from polycrystalline boron doped diamond show clear evidence of superconductivity with critical temper-

atures in the Kelvin range and critical field in the Tesla range. Such robust superconducting properties in these superhard materials make them promising candidates for superconducting nanoelectromechanical systems.

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1 Introduction The huge interest seen in the special class of superconducting materials belonging to the covalent metals started with the discovery of superconductivity in MgB₂ [1]. Ekimov et al. [2] in 2004 reported the superconducting properties of boron doped diamond for the first time. This led to the study of superhard superconducting materials [3, 4]. Apart from the mechanism of superconductivity in these systems, which remain largely unexplored, the very high Young's modulus of boron doped diamond makes it a front runner for making nanoelectromechanical systems (NEMS) of exceptional high quality factor. Before realizing any NEMS from boron doped diamond it is, however, essential to prove that both the qualities of this system, i.e. superconductivity [5–7] and mechanical properties [8], are preserved when nanocrystalline layers grown on non-diamond substrate are nanopatterned. Earlier studies in this system have concentrated their attention towards the bulk properties of this system. Hence, it is quite essential to investigate the properties of nanostructured boron doped diamond.

In this paper, a comprehensive study of nanostructured superconducting polycrystalline diamond films is presented. It is shown that these nanostructures have superconducting

critical parameters like transition temperature and critical field comparable to that of bulk materials.

2 Experimental The nanocrystalline boron-doped diamond was obtained by chemical vapour deposition on a silicon oxide wafer. Before depositing the thin films, the wafers were cleaned with NH₃OH/H₂O₂/H₂O (1:1:5) solution at 75 °C for 10 min, and rinsed in pure DI water in an ultrasonic bath. Nucleation enhancement on wafers was achieved by seeding the wafer with diamond nanoparticles from an aqueous colloid of monodisperse diamond particles known to have sizes less than 7 nm in solution as confirmed by dynamic light scattering [9, 10]. Atomic force microscope (AFM) measurements have shown this technique to result in uniform nucleation densities far in excess of 10¹¹ cm⁻². Diamond growth was then performed by microwave plasma enhanced chemical vapour deposition (MPCVD) from 4% CH₄ diluted in H₂ with additional boron from a trimethylboron gas source. A microwave power of 3000 W at 60 mbar, was used with substrate temperature being around 800 °C as monitored *in situ* with a bichromatic pyrometer.

The nanostructures were made using electron beam lithography technique. In Fig. 1, the lithography process is

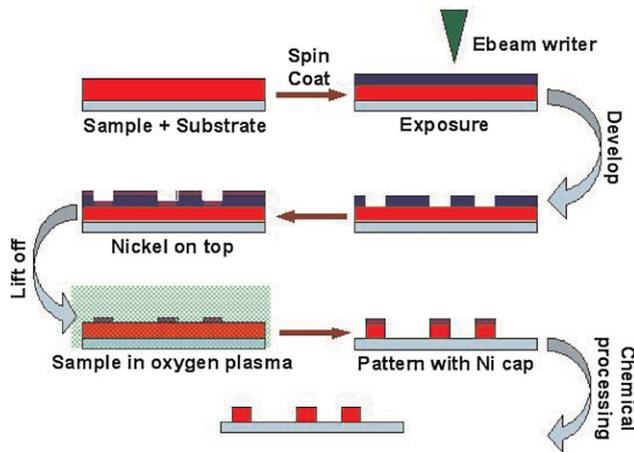


Figure 1 (online colour at: www.pss-a.com) Schematics of the nanofabrication process.

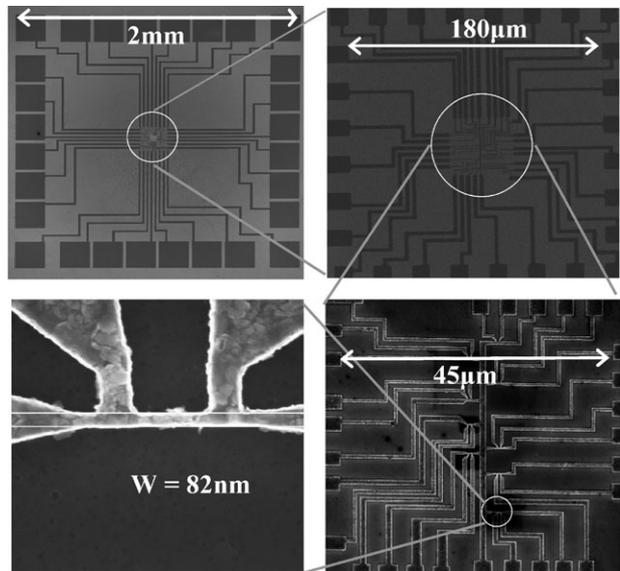


Figure 2 The SEM images of a typical microcircuit fabricated by electron beam lithography.

1 shown. The wafer was spin coated with 4% polymethyl-
 2 methacrylate (PMMA) to form a 250 nm thick layer which
 3 was prebaked at 180 °C for 5 min. This PMMA layer was
 4 exposed to electron beam with a dose of $360 \mu\text{C cm}^{-2}$ for an
 5 acceleration voltage of 20 kV. For the development of the
 6 exposed wafer, the wafer was dipped in 1:3 solution of
 7 methyl isobutyl ketone (MIBK) and isopropyl alcohol (IPA)
 8 for 1 min. A thin layer of nickel (65 nm) was then deposited
 9 and patterned using a standard electron-gun evaporator and
 10 lift-off technique. This was followed by plasma etching of
 11 diamond structures using electron cyclotron resonance
 12 oxygen plasma [11] and a -27 V dc bias for ≈ 8 min. This
 13 leads to an etching rate of $\approx 40 \text{ nm/min}$. The nickel layer
 14 acted as a mask in this process. The nickel layer was removed
 15 using FeCl_3 solution and ohmic contacts were then obtained
 16 by an evaporation of metals (Ti–Au).

17 In Fig. 2, a typical microcircuit fabricated by electron
 18 beam lithography technique is shown. The bottom left panel
 19 in the figure shows the picture of the line with the smallest
 20 width $\approx 80 \text{ nm}$, which is $\approx 500 \text{ nm}$ long and $\approx 300 \text{ nm}$ thick.
 21 Note that in this case the aspect ratio is as high as $\sim 1:3$, the
 22 anisotropy of the plasma etching allowing to pattern one
 23 single grain. The top and bottom right panels are blow up of
 24 $200 \times 200 \mu\text{m}^2$ and $50 \times 50 \mu\text{m}^2$ area in the centre of the
 25 microcircuit, respectively.

26 **3 Results and discussion** In Fig. 3, the resistance of
 27 an unpatterned thin film as a function of temperature is
 28 shown. Four silver paste electrical contacts were deposited
 29 on the surface of as-grown layer for this measurement. A
 30 standard ac lock-in technique with a very low current
 31 injection of $1 \mu\text{A}$ was used for this measurement. The data
 32 clearly show a superconducting transition with a zero
 33 resistance at $\approx 3.5 \text{ K}$. The width of the transition is quite
 34 large, typically 0.7 K with a 10–90% of the onset resistance
 35 criterion. In the inset of the same figure a scanning electron
 36 microscope (SEM) picture of the sample with grains of
 37 typical size $\approx 250 \text{ nm}$, for a film thickness of $\approx 300 \text{ nm}$ is

shown. The large width of transition seen in the resistivity
 data is attributed to the distribution of the grain sizes across
 the sample.

In Fig. 4a and b, the current–voltage characteristic (V – I
 curve) and the calculated differential resistance for a 350 nm
 wide and 500 nm long wire is shown. The inset in the panel
 (a) shows the critical temperature of a few representative
 wires of varying widths. These measurements were
 performed in both a ^3He and a $^3\text{He}/^4\text{He}$ dilution refrigerators.
 The current through the sample for these measurements were
 100 nA for the 500 nm wide wire and 10 nA for the rest of the

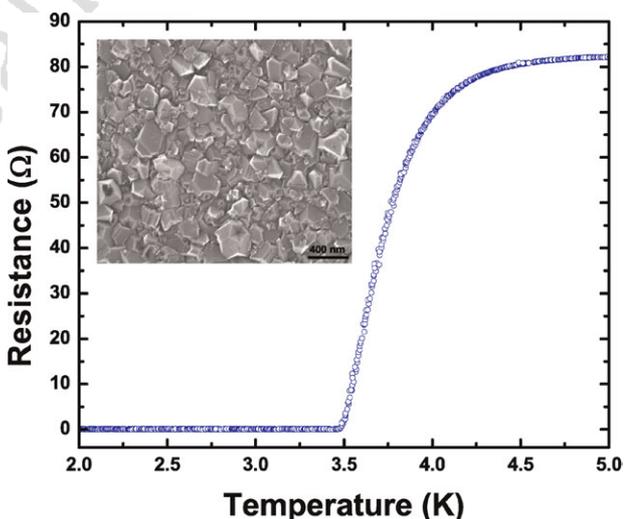


Figure 3 (online colour at: www.pss-a.com) Superconducting resistive transition in a boron-doped diamond thin film. The inset is a SEM image of the surface of the sample, consisting of grains of typically $\approx 250 \text{ nm}$.

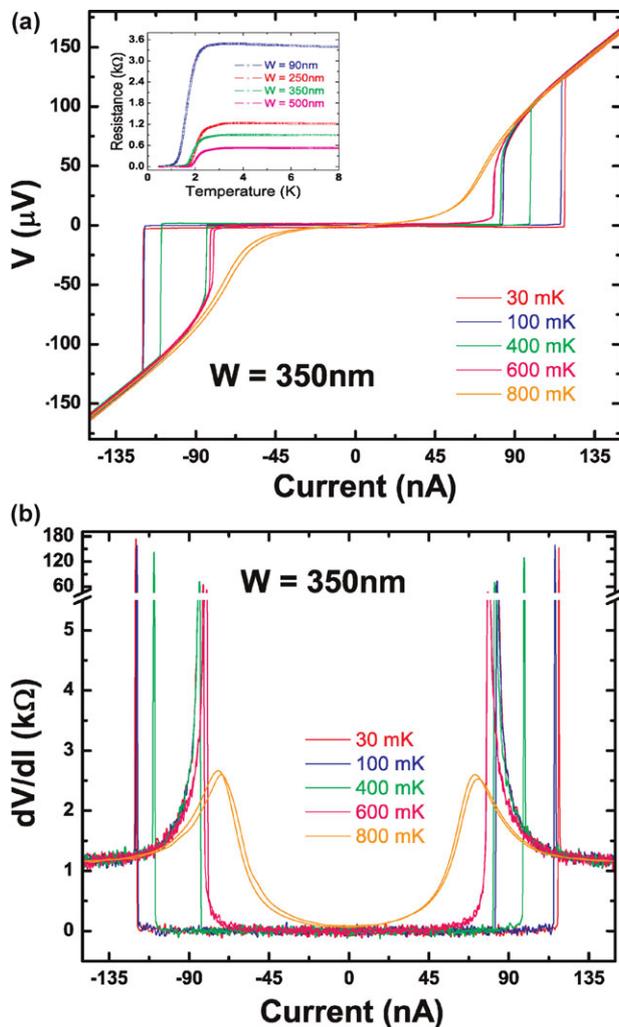


Figure 4 (online colour at: www.pss-a.com) (a) Voltage–current (V – I) characteristic of a 350 nm wide wire at different temperatures. The V – I curves are hysteretic due to thermal effect (Joule heating). The inset shows the R versus T curves for four representative wires. (b) Differential resistance extracted from the V – I curves. The resistance goes to zero when the wire is in its superconducting state.

1 wires. For the measurement of the V – I curves, we have used a
 2 standard four probe dc technique. No significant difference
 3 was observed from the critical temperature measured on the
 4 ‘bulk’ sample (≈ 2.5 K for this wafer) except for the case of
 5 the narrowest wire (below 100 nm wide, $T_c \approx 1.7$ K). This
 6 was seen for all our superconducting diamond thin films: the
 7 critical temperature of the wires were those of the bulk
 8 material except for the cases where the wire width is less than
 9 100 nm. The V – I curves in panel (a) are hysteretic due to
 10 thermal effect: when the critical current is reached, Joule
 11 effect heats up the wire and the critical current measured
 12 when subsequently decreasing the current is thus much lower
 13 than the critical current measured when increasing the current
 14 [12, 13]; moreover, this ‘retrapping’ current is

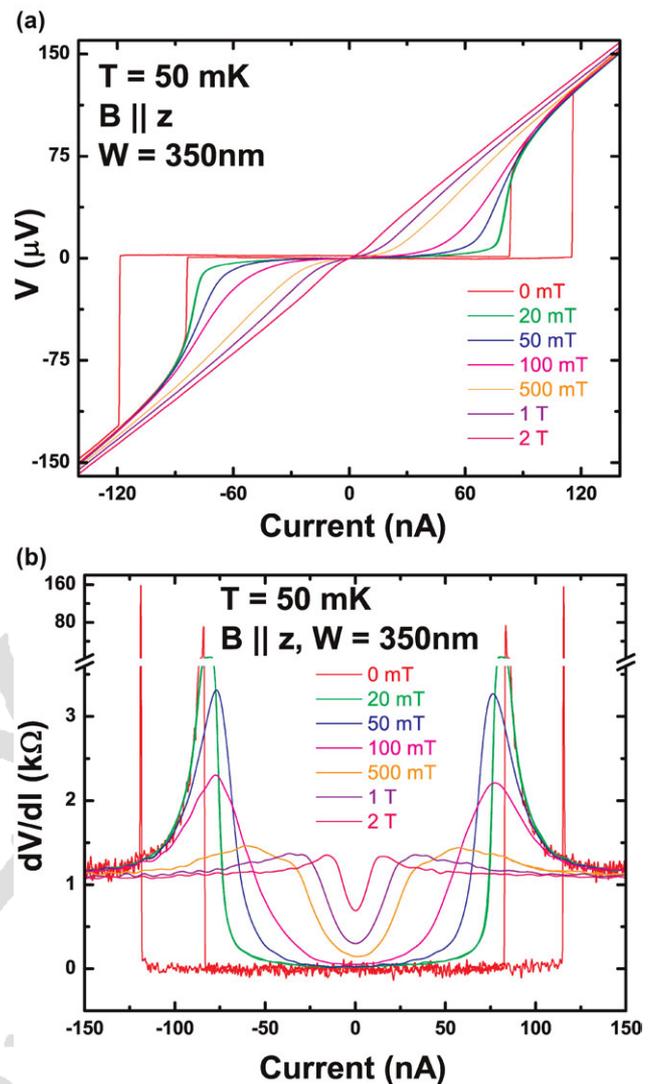


Figure 5 (online colour at: www.pss-a.com) (a) Voltage–current (V – I) characteristic of a 350 nm wide wire at 50 mK under different magnetic fields. The field is applied perpendicular to the plane of the sample. The behaviour is hysteretic until the applied field reaches 20 mT. (b) Differential resistance extracted from the V – I curves. The resistance goes to zero when the applied field is below 100 mT.

1 independent of the temperature of the refrigerator, as the
 2 actual temperature of the sample is then fixed by the dc
 3 current through the wire.

4 The critical field of this sample was also measured by
 5 applying magnetic field in and out of plane of the sample. In
 6 Fig. 5a and b, the V – I characteristics and differential
 7 resistance for a 350 nm wide wire under different magnetic
 8 fields and at 50 mK is shown. The critical current decreases
 9 when the applied magnetic field is increased. Further, it is to
 10 be noted that the V – I characteristic is no more hysteretic
 11 once the field goes beyond 20 mT. In this case, the Joule
 12 heating becomes negligible due to the lowering of the critical
 13 current. The derivatives of the V – I characteristics were
 14 calculated and the differential resistance of the data is shown

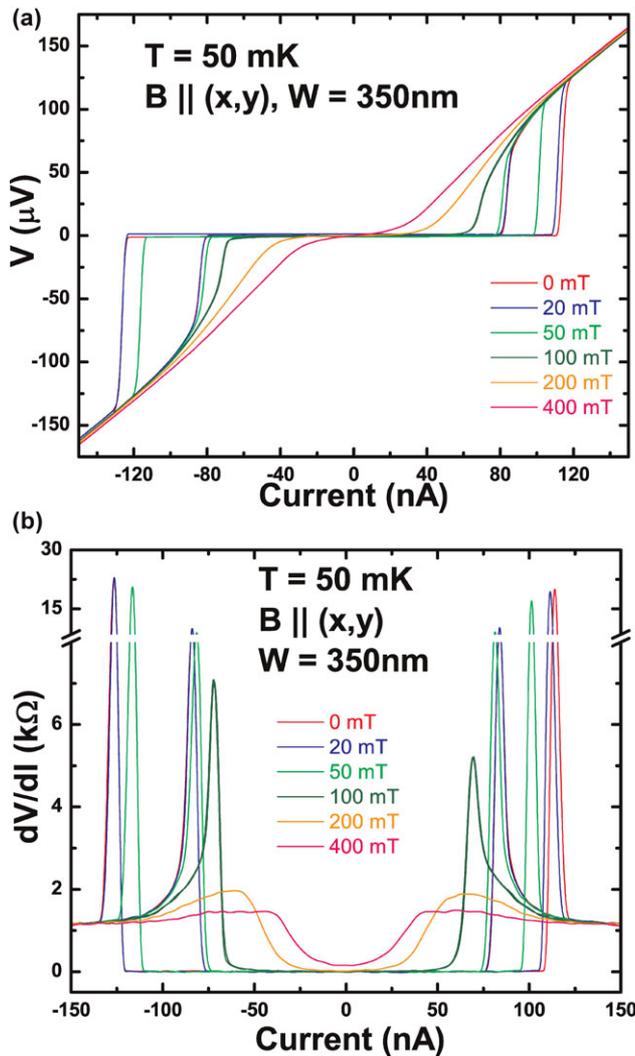


Figure 6 (online colour at: www.pss-a.com) (a) Voltage–current ($V-I$) characteristic of a 350 nm wide wire at 50 mK under different magnetic fields. The field is applied in the plane of the sample. The behaviour is hysteretic until the applied field reaches 80 mT. (b) The differential resistance extracted from the $V-I$ curves. The resistance goes to zero when the whole wire is in its superconducting state.

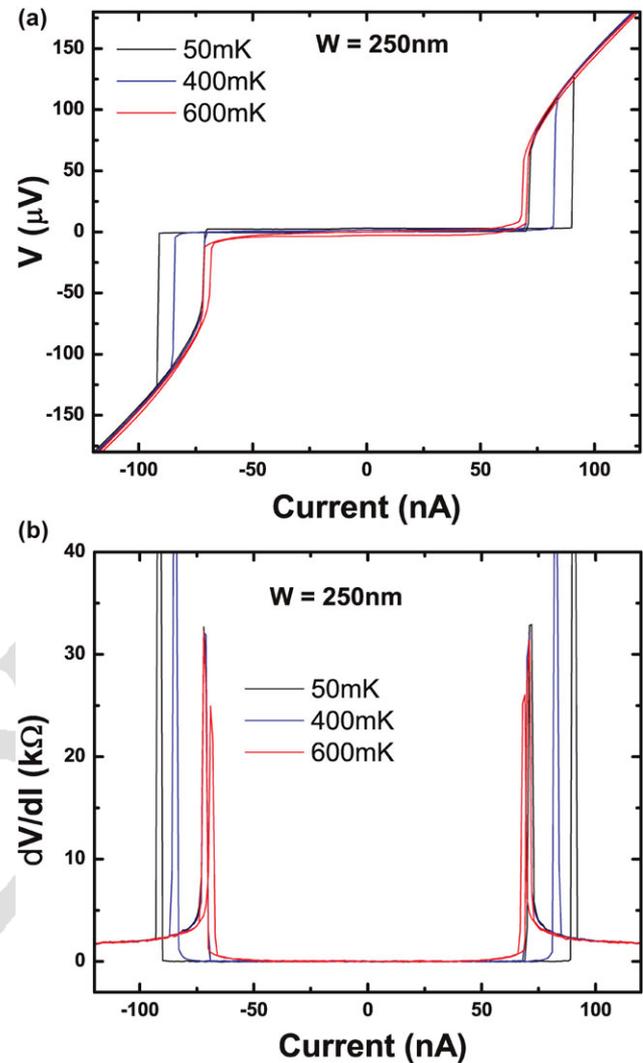


Figure 7 (online colour at: www.pss-a.com) (a) Voltage–current ($V-I$) characteristic of a 250 nm wide wire at different temperatures. The $V-I$ curves are hysteretic due to thermal effect. (b) Differential resistance extracted from the $V-I$ curves.

1 in Fig. 5b. One can see that when the applied field is smaller than 100 mT a clear zero is observed around $I=0$. Now, when the field is increased further, a clear dip near the zero current even for applied fields as high as 2 T is seen. This shows that there are still pockets of superconductivity in the nanowires at such high fields. The most likely explanation would be that some grains in the wires remain superconducting even at such high magnetic field.

2 In Fig. 6a and b, the $V-I$ characteristics and the differential resistance of the 350 nm wide wire when the applied field is in the plane of the sample and perpendicular to the current through the sample is shown. In this case, the hysteresis in the sample was completely removed only when the field was above 80 mT. So this means, that for the same

1 applied field, the critical current is higher for the case when the applied field is in the plane of the sample. We do not have any definitive explanation to this effect but it is quite possible that the introduction of vortices plays a key role in the determination of the critical field. In this case, the difference in aspect ratio of the devices when applying the field perpendicular to the structures or in the plane of the structures may account for the observed behaviour. The differential resistance calculated for this configuration (shown in Fig. 6b) shows that there is distinct zero in the resistance even at fields as high as 200 mT.

2 In Fig. 7a and b, the $V-I$ characteristics and the calculated differential resistance, respectively, are shown for a 250 nm wide and 500 nm long wire. The wire shows hysteresis due to

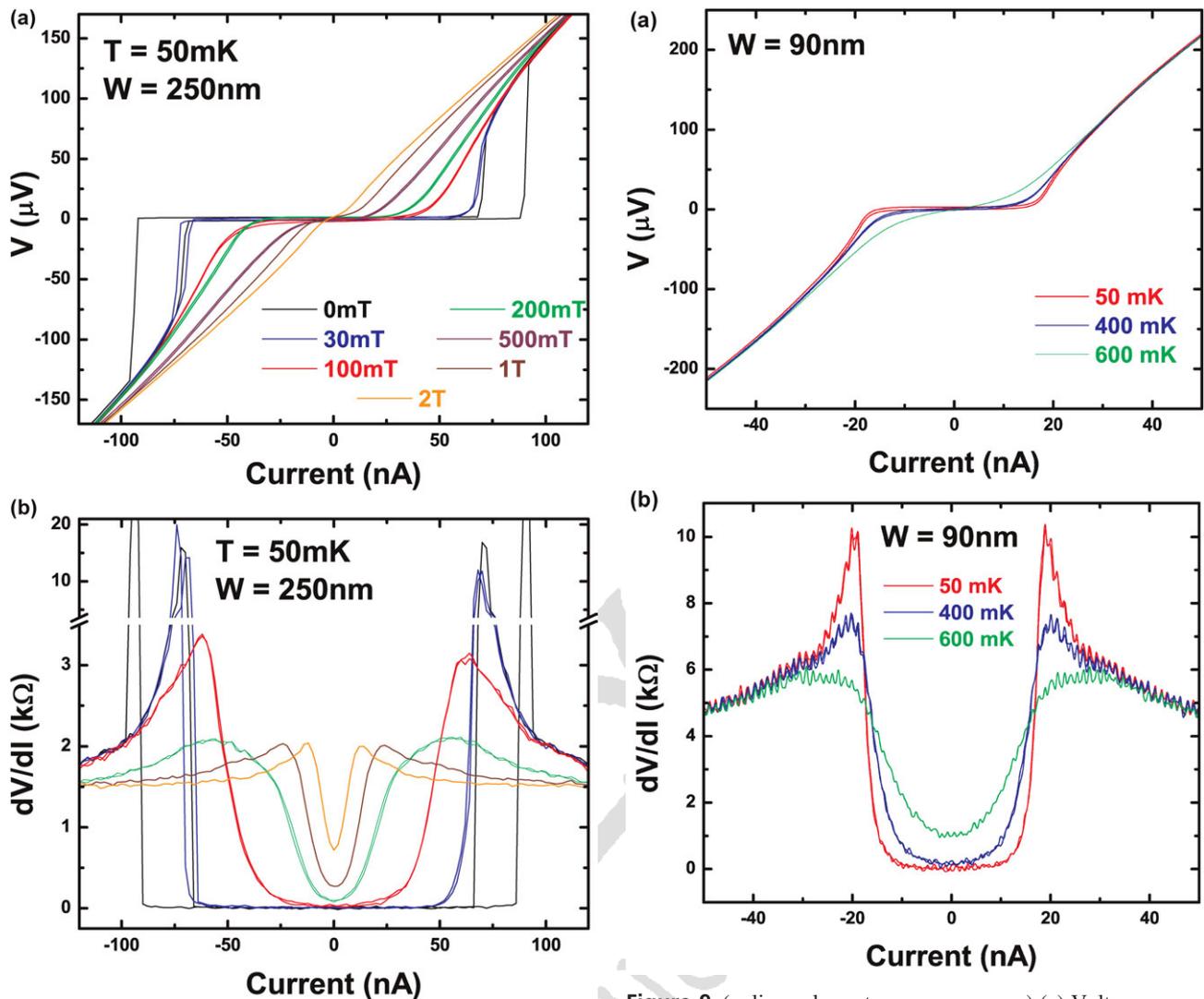


Figure 8 (online colour at: www.pss-a.com) (a) Voltage–current ($V-I$) characteristic of a 250 nm wide wire at 50 mK under different magnetic fields. The field is applied perpendicular to the plane of the sample. The behaviour is hysteretic until the applied field reaches 30 mT. (b) Differential resistance extracted from the $V-I$ curves. The resistance goes to zero when the applied field is below 100 mT. The legends for this panel is same as that for (a).

Figure 9 (online colour at: www.pss-a.com) (a) Voltage–current ($V-I$) characteristic of a 90 nm wide wire at different temperatures. (b) Differential resistance extracted from the $V-I$ curves. The resistance goes to zero when the wire is in its superconducting state.

1 thermal effects until the temperature reaches 600 mK. The
 2 retrapping current in this case is of the order of 70 nA while
 3 for 350 nm wire it was 83 nA. If one defines the retrapping
 4 power as $I_r^2 R_r$, where I_r is the retrapping current and R_r is the
 5 retrapping resistance, then for a given sample this quantity
 6 should be constant. To check this fact with our experimental
 7 data, we compare the retrapping powers of two wires of
 8 different widths. Since in the nanowires presented in this
 9 paper the lengths and the thicknesses are constant one can say
 10 that the ratio of the widths of any two wires should be equal to
 11 the ratio of the squares of their respective retrapping currents.

1 When one compares these ratio for the 350 and 250 nm wire,
 2 it is seen that the ratio of the widths is 1.4 which is similar to
 3 the ratio of the squares of the retrapping current for the
 4 corresponding wires. Hence, we can conclude that the
 5 retrapping power is an intrinsic property of the sample.

6 In Fig. 8a and b, the field dependence of critical current
 7 and differential resistance at a fixed temperature of 50 mK
 8 for the 250 nm wide wire is shown. One can see that the
 9 curves are hysteretic but the hysteresis disappears on
 10 applying a magnetic field of 30 mT. The differential
 11 resistance plotted in panel (b) of the same figure reveals
 12 the presence of few grains (as seen for 350 nm wide wire as
 13 well) having critical field above 2 T.

14 In Fig. 9a and b, the $V-I$ characteristics and differential
 15 resistance respectively, of a 90 nm wide and 500 nm long
 16 wire as a function of temperature is shown. Here the

1 characteristic is not hysteretic. This can be explained as
2 follows. The retrapping power for this sample is ~ 4.5 pW.
3 For 90 nm wide wire, the power dissipated at the critical
4 current at 50 mK is equal to 0.65 pW, which is much less than
5 the retrapping power and hence the hysteretic behaviour is
6 not seen. The differential resistance plotted in panel (b)
7 shows that the sample is completely superconducting below
8 400 mK and above this temperature, the wire remains in the
9 superconducting transition region until it reaches a tempera-
10 ture of ~ 1.7 K (inset of Fig. 4).

11 **4 Conclusion** In conclusion, nanostructures from
12 boron-doped nanocrystalline superconducting diamond has
13 been successfully fabricated. Using electron beam lithogra-
14 phy, devices of characteristic size less than 100 nm and aspect
15 ratio as high as 1:3 have been prepared. These structures have
16 critical temperatures in the Kelvin range, similar to what is
17 observed in ‘bulk’; only a slight decrease of T_c is observed
18 for wires thinner than 100 nm. Critical fields close to 100 mT
19 were measured and traces of superconductivity were
20 observed even under magnetic fields as strong as 2 T. The
21 experiments also revealed that there is stronger suppression
22 of critical properties when the applied magnetic field is
23 perpendicular to the sample plane. This study proves that
24 superconductivity in boron-doped diamond is a very robust
25 phenomenon which makes it a promising candidate for
26 future applications in the field of superconducting nanoelec-
27 tro-mechanical systems.

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